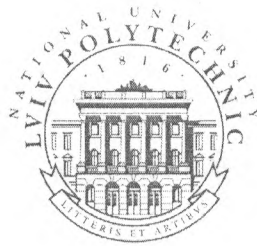




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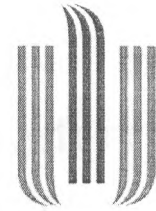
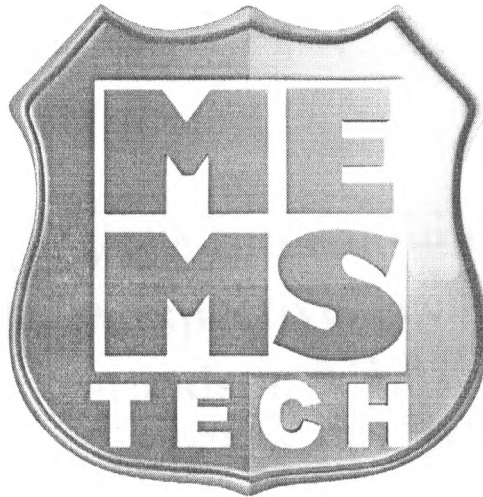
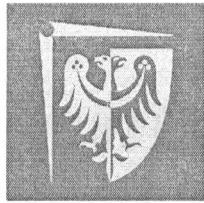
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# Investigation and Animation of Spring Dynamic Absorber

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**Abstract**—Animations of complex mechanical systems with repetitive movements of interest in terms of activation of imagination in their study and research. Action of the spring dynamic absorber, investigation of the physical quantities of proposed mathematical model was implemented using non-linear Runge-Kutta type methods. Two kinds of methods: a nested method of relative accuracy 3(2) and two-sided method with accuracy 2 are consruted in proposed paper. Also estimation of main term of local error are obtained. For all these algorithms, in contrast to other algorithms, only three calls to the right-hand side of the differential equation are required.

**Keywords**—spring dynamic vibration absorber, animation, Cauchy problem, nonlinear approximation, continued fractions, two-sided methods.

## I. INTRODUCTION

For investigation of applied mechanics problems it is useful to use modern mathematical modeling of vibrating technological systems [1]. The main problems of the dynamics for nonlinear oscillatory systems are the ability to create accurate analytical methods for studying such systems [2] only for a very limited class of mathematical models. Therefore, it is still urgent to create and develop new computational methods that allow to study, analyze and optimize the parameters of a wide range of vibrating technological systems. An important area of research in this topic is the synthesis and optimization of the parameters for mechanical vibration dampers, which are now widely used [3]. They are designed for dampen vibrations of mechanisms, machines [4], building structures. Also, when studying the parameters of dynamic systems and calculating the strength of the structure, it is important to take into account the influence of adverse environmental factors [5, 6].

In the study of known designs of mechanical oscillation valves, it is necessary to provide the relationship that combines the dynamics of linear and nonlinear oscillations with their structural and mechanical characteristics. On the basis of the received mathematical formulas it is possible to set new optimization problems.

The purpose of the study is to construct a mathematical model of a passive elastic dynamic dampener and to investigate the behavior of dynamic systems using two-sided methods. The investigated mechanical vibration dampers belong to two-mass mechanical systems. Such systems are being actively researched with the aim to optimize them. In [7], a parameter extension method for vibration impact systems while modeling the impact of contact force, was developed, theoretical calculations were designed for two-mass systems with two degrees of freedom. In [8] studies were conducted to reduce the noise of internal combustion engines by means of mechanical damping devices and the design of one of the possible variants of such device was developed. In [9, 10] the pendulum dumbbell type damper is investigated and it is proposed to adjust the natural frequency of the pendulum dampener with the help of optimal choice of design dimensions. In [11-15], investigations of cylindrical, dynamic mechanical vibration dampers, methods of protection against vibrations and shocks were carried out.

Since fractional-rational methods along with two-sided methods give good convergence of algorithms, they were used for research in the proposed work [16-18].

## II. FORMULATION OF THE PROBLEM

The motion of a two-mass system of a passive spring dynamic vibration absorber [7] (Fig. 1) is described by a system of two second-order differential equations, which can be we reduce to four first-order differential equations with zero initial values:

$$\begin{aligned} \frac{dx_1}{dt} &= v_1, & \frac{dx_2}{dt} &= v_2, \\ \frac{dv_1}{dt} &= Q(t)/m_1 - (\omega_1^2 x_1 + \omega_2^2 (x_1 - x_2) + 2r_1 v_1), \\ \frac{dv_2}{dt} &= \omega_2^2 (x_1 - x_2) - 2r_2 v_2. \end{aligned} \quad (1)$$

Now we need to find a solution to this system, as well as to investigate and analyze the physical quantities of the spring dynamic absorber and create an animation program for the dynamic system of a passive spring damper.

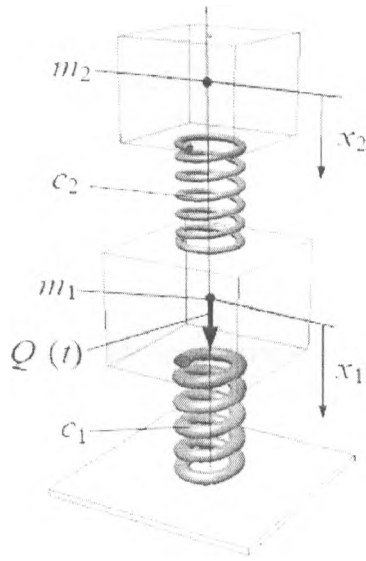


Fig. 1 The passive dynamic spring vibroabsorber

### III. CONSTRUCTION OF THE THIRD-ORDER ACCURACY METHOD

Consider problem (1) in a more general formulation, namely, as a Cauchy problem for system of differential equations:

$$\frac{d\bar{u}}{dt} = \bar{f}(t, \bar{u}), \quad \bar{u}(t_0) = \bar{u}_0, \quad t \in [t_0, t_0 + T], \quad (2)$$

where

$$[t_0, t_0 + T] \subset R, \quad \bar{u}(t) \in R^S, \\ \bar{f}: [t_0, t_0 + T] \times R^S \rightarrow R,$$

and  $\bar{f}$  has the necessary smoothness for the calculations.

Since the proposed method is component in nature, for simplicity, we can consider one differential equation.

According to the theory of construction of one-step Runge-Kutta methods [19], we will look for a numerical solution of the corresponding Cauchy problem in the form of expansion of the exact solution by means of continuous fractions [20]:

$$y_{n+1}^{[k,l]} = u_n / \Psi_n^{[k,l]}, \quad (3)$$

where

$$\Psi_n^{[k,l]} = \sum_{i=0}^{k-1} \psi_{i,0} + \frac{\psi_{k,0}}{1 + \frac{\psi_{k,1}}{1 + \dots + \frac{\psi_{k,l-1}}{1 + \psi_{k,l}}}} \quad (4)$$

If  $k+l=3$  ( $k=1,2,3; l=0,1,2$ ), then the expressions for  $\psi_{k,l}$  are of the form:

$$\psi_{i,0} = -\frac{\sigma_m}{u_n} \sum_{m=1}^i \psi_{i-m,0}, \quad i = \overline{1,3}; \quad u_n \neq 0,$$

$$\psi_{2,1} = -\frac{\psi_{3,0}}{\psi_{2,0}}, \quad \psi_{1,2} = \psi_{2,1} - \psi_{1,1}.$$

$$\sigma_m = \tau \cdot \sum_{i=1}^3 c_{mi} k_i, \quad k_i = f(t_n + a_i \tau, u_n) + \tau \sum_{j=1}^{i-1} b_{ij} k_j,$$

$$a_1 = 0, \quad a_i = \sum_{j=1}^{i-1} b_{ij}. \quad (5)$$

Here  $\tau$  – integration step ( $\tau = t_{n+1} - t_n, n = 0, 1, 2, \dots$ ),  $c_{mi}$  ( $m, i = \overline{1,3}$ ),  $a_i, b_{ij}$  ( $i = \overline{2,3}; j = \overline{1, i-1}$ ) parameters.

**Theorem.** If parameters  $c_{mi}$  ( $m, i = \overline{1,3}$ ),  $a_i, b_{ij}$  ( $i = \overline{2,3}; j = \overline{1, i-1}$ ) satisfy the system of algebraic equations

$$\sum_{i=1}^3 c_{1i} = 1, \quad \sum_{j=1}^3 c_{ij} = 0, \quad i = \overline{2,3},$$

$$\frac{1}{2} - \sum_{i=2}^3 c_{1i} a_i - \sum_{i=2}^3 c_{2i} a_i = 0, \quad \sum_{j=2}^3 c_{3j} a_j = 0,$$

$$\frac{1}{6} - \sum_{m=2}^3 \sum_{i=2}^3 c_{mi} \frac{a_i^2}{2} = 0, \quad a_i = \sum_{j=2}^{i-1} b_{ij}, \quad (i = \overline{2,3}),$$

$$\frac{1}{6} - \sum_{m=2}^3 \sum_{i=2}^3 c_{mi} \sum_{j=2}^{i-1} b_{ij} a_i = 0, \quad (6)$$

then there is an assessment

$$R_{n+1}^{[k,l]} = u(x_{n+1}) - u_{n+1}^{[k,l]} = O(\tau^4). \quad (7)$$

This system has three families of solutions. Here is one of them:

1) If  $a_2 \cdot a_3(a_3 - a_2)(a_2 - 2/3) \neq 0$ , then

$$c_{11} = 1 + \frac{2 - 3(a_2 + a_3)}{6a_2 a_3} - c_{33} \frac{a_3 - a_2}{a_2} + c_{22} + c_{33}, \\ c_{12} = \frac{3a_3 - 2}{6a_2(a_3 - a_2)} + c_{31} \frac{a_3}{a_2} - c_{22}, \\ c_{13} = \frac{2 - 3a_2}{6a_3(a_3 - a_2)} - c_{23} - c_{33}, \quad (8) \\ c_{21} = -c_{22} - c_{23}, \quad c_{31} = c_{33} \frac{a_3 - a_2}{a_2},$$

$$c_{32} = -\frac{a_3}{a_2} c_{33}, \quad b_{21} = a_2,$$

$$b_{32} = \frac{a_3(a_3 - a_2)}{a_2(2 - 3a_2)}, \quad b_{31} = a_3 - b_{32},$$

where  $c_{22}, c_{23}, c_{33}, a_2, a_3$  parameters:

In particular, if put  $c_{ii} = 0$  for  $j > i$ , we will obtain respectively:

$$\text{a) } c_{11} = 1, \quad c_{21} = -\frac{1}{2a_2}, \quad c_{12} = c_{13} = 0,$$

$$c_{22} = \frac{1}{2a_2}, \quad c_{23} = 0, \quad c_{31} = \frac{2 - 3a_2}{6a_2 a_3}$$

$$c_{32} = \frac{3a_2 - 2}{6a_2(a_3 - a_2)}, \quad c_{33} = \frac{2 - 3a_2}{6a_3(a_3 - a_2)} \quad (9)$$

$$b_{21} = a_2, \quad b_{32} = \frac{a_3(a_3 - a_2)}{a_2(2 - 3a_2)}, \quad b_{31} = a_3 - b_{32}$$

#### IV. SECOND ORDER OF ACCURACY METHODS WITH TWO-SIDED ESTIMATION OF LOCAL ERROR

We construct a two-sided method. Consider formulas (3)-(5) for  $k=3, l=0$  and put

$$c_{11} = 1, \quad c_{12} = c_{13} = c_{23} = 0, \quad a_2 = b_{21}, \quad a_3 = b_{31} + b_{32}.$$

Let us write three sets of parameters that give a two-sided estimation of the solution at each nodal point:

$$I. \quad c_{21} = \frac{1 + \gamma^{[+]}}{2a_2}, \quad c_{22} = \frac{1 + \gamma^{[-]}}{2a_2},$$

$$c_{31} = \frac{2 + 3(\gamma^{[+]}a_3 - a_2)}{6a_2a_3}, \quad c_{32} = \frac{3a_2 - 2 - 3\gamma^{[-]}(a_3 - a_2)}{6a_2(a_3 - a_2)},$$

$$c_{33} = \frac{2 - 3\alpha_2}{6\alpha_3(\alpha_3 - \alpha_2)}, \quad b_{21} = a_2,$$

$$b_{32} = \frac{a_3 \cdot a_3 - a_2}{a_2 \cdot 2 - 3a_2}, \quad b_{31} = a_3 - b_{32}, \quad (10)$$

moreover  $a_2 a_3 (a_3 - a_2) (2 - 3a_2) \neq 0$ .

Local error of these formulas looks like :

$$R_{n+1}^{[3,0]} = \gamma^{[+]} \tau^2 k_1 (k_2 - k_1) / (a_2 u_{n-1}) + O(\tau^4). \quad (11)$$

These formulas that correspond to two values of  $\gamma^{[+]}$  are two-sided formulas and differ only in sign, one of which gives the upper approximation and the other the lower approximation. As an approximate solution, the half-sum of these two-sided approximations is taken.

The proposed algorithm allows us to find several approximations to the exact solution, comparing which we can get useful information for selection of the integration step.

#### V. INVESTIGATION RESULTS

The calculations were carried out in the Mathcad package. Initial data (Fig.1) :

$m_1 = 100 \text{ kg}$ ,  $m_2 = 10 \text{ kg}$  – masses of the system of bodies,  
 $c_1 = 10 \text{ N/m}$ ,  $c_2 = 1 \text{ N/m}$  – stiffness of springs,  
 $\beta_1 = 1.5 \cdot 10^{-1} \text{ kg/s}$ ,  $\beta_2 = 1.5 \cdot 10^{-1} \text{ kg/s}$  – oscillation damping parameters,  
 $H = 10 \text{ N}$  – amplitude of disturbing force,  
 $f = 0.05 \text{ Hz}$  – frequency of disturbing force.

Formulas for calculation:

$$\omega_1 = \sqrt{c_1/m_1}, \quad \omega_2 = \sqrt{c_2/m_2},$$

$$r_1 = \beta_1 / (2m_1), \quad r_2 = \beta_2 / (2m_2),$$

$$h = H/m_1, \quad \omega = 2\pi f. \quad (12)$$

The disturbing force is related to the mass,  
 $f(t) = Q(t)/m_1 = h \sin(\omega t)$ .

In our model it is assumed that the resistance of the medium is negligible and has little effect on the resonant frequencies of the dampers and bodies of mass  $m_1$ , whose damping oscillations are being investigated.

Graphical representation of numerical solutions positions and velocities of bodies of mass  $m_1$  and  $m_2$  (Fig. 2- Fig. 5). From the graphs presented in Fig. 2 and Fig. 3, we see that the amplitude and velocity of the body with mass  $m_1$  reduced.

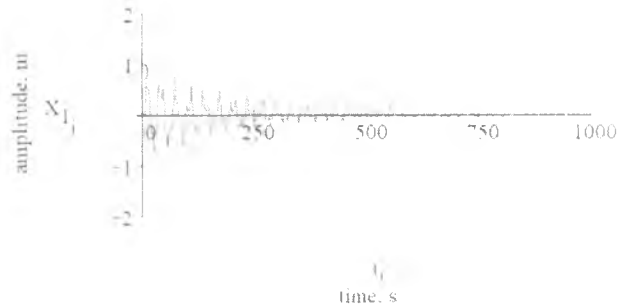


Fig. 2 Graph of the amplitude of oscillations of the body with mass  $m_1$

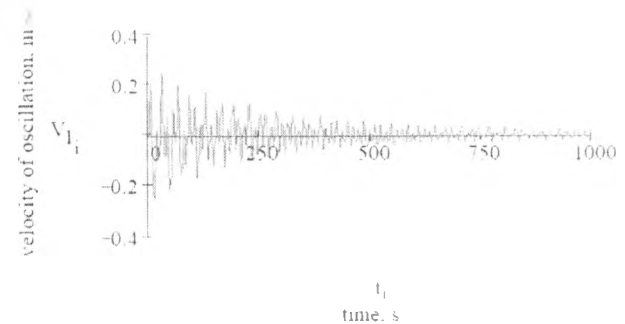


Fig. 3 Graph of the velocity of oscillations of the body mass  $m_1$

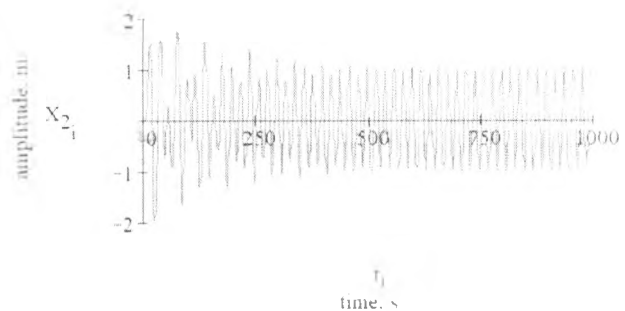


Fig. 4 Graph of amplitude of oscillations of the damper (body mass  $m_2$ )

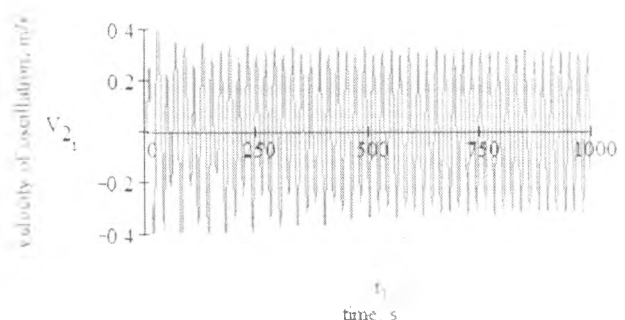


Fig. 5 Graph of the speed of oscillations of the damper

The amplitude of oscillations and velocities of the body mass  $m_2$  (vibration dampener) is stabilized at a certain level and shifts in phase relative to the oscillations of the body  $m_1$  (Fig. 4, 5), which can be observed in the animation and there is a redistribution of energy between the body and the oscillator dampener – energy goes to the mass dampener  $m_2$  (Fig. 6).

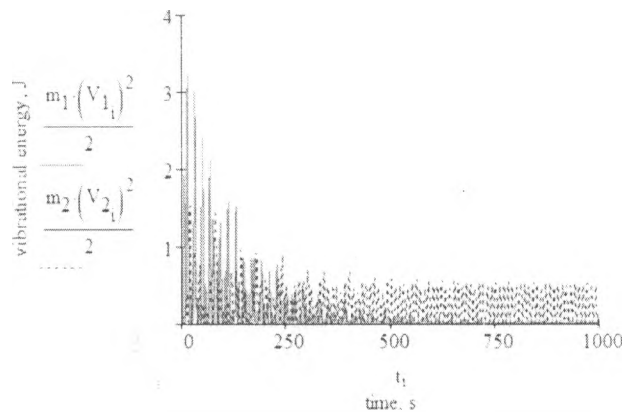


Fig. 6. Fluctuation energy transition from the body of mass  $m_1$  to the body mass  $m_2$

Initially, both bodies oscillate by the phase shift  $\approx 0$ , and at the moment of maximum damping of oscillations, the oscillation dampener moves in opposite phase to the mass  $m_1$ .

Compiled a program for animation of dynamic system a passive spring absorber [21].

## VI. CONCLUSION

Action of a spring dynamic absorber using the proposed methods, as well as the constructed model were investigated on animation in Mathcad.

The third-order accuracy method is constructed, as well as the second-order accuracy formulas, which at each integration point give an approximation to the exact solution with excess and deficiency.

Without additional calculation of the right-hand side of the differential equation, we obtain the estimation of the local error principal term.

Derived two-sided formulas allow at each step of integration to reduce the number of appeals to the right hand-side of the differential equation by 25% compared to the traditional two-sided Runge-Kutta methods [22-25].

The obtained program makes it possible to simulate the operation of the spring dynamic absorber under different external influences, not only with harmonic periodic force, but also with shocks, vibrations with different nature and law of the resistance of the environment.

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